



## **SUBSTANTIATE THE COVERAGE WIDTH OF A COMPREHENSIVE CHISEL CULTIVATOR**

M. T. Mansurov

Doctor of Technical Sciences, Namangan Engineering Construction Institute,  
Namangan, Republic of Uzbekistan, E-mail: m\_mansurov\_1978@mail.ru

N. T. Nabixo'jaeva

Basic doctoral student of the Research Institute of Agricultural Mechanization

B. U. Toshpulatov

PhD, Namangan Engineering Construction Institute,  
Namangan, Republic of Uzbekistan

### **Annotation**

This article provides information on the development of a comprehensive chisel cultivator and the results of theoretical research to determine its coverage. Based on the results of calculations, the coverage width of the chisel cultivator for aggregation with tractors ARION-630C, AXION-850, ARES-697 and NewHolland T7060 is in the range of 4.6-5.8 m, for tractors "Magnum" 8940, MX-255, It should be 7,2 m.

**Keywords:** Chisel-cultivator, coverage width, gravity resistance, softener claw, story claw.

### **Introduction**

Based on the results of research on improving the agro-technical performance of existing chisel cultivators, reducing material and energy consumption, as well as the analysis of scientific and technical literature, a comprehensive design scheme and technological process of chisel cultivator was developed.

The comprehensive chisel-cultivator is designed as a suspension and consists of a central (1) and two lateral (right 2 and left 3) sections.

The side sections are connected to the central section by longitudinal hinges, which are transferred from the working position to the transport position and from the transport position to the working position by means of hydraulic cylinders [1].



## Research Methods

We determine the coverage width of the chisel cultivator by the following expression [2].

$$B \leq \chi \frac{P_H}{q}, \quad (1)$$

in this  $\chi$  – tractor traction utilization factor;  $P_H$  – rated traction power of the tractor, H;  $q$  – the specific gravity of the chisel cultivator, ie the resistance corresponding to the width of one meter, H.

## Results

The traction resistance of a chisel cultivator is mainly due to the traction resistance of its working bodies. Therefore, its specific resistance to gravity can be determined with sufficient accuracy by the following expression

$$q = \frac{R_1 + R_2}{2a_k}, \quad (2)$$

in this  $R_1, R_2$  – traction resistance of the working bodies mounted on the first and second rows of the chisel-cultivator, ie the softener and axial claws, respectively, H;  $a_k$  – width between traces of working bodies, m.

Given expression (2), expression (1) has the following appearance

$$B \leq 2\chi \frac{P_H a_k}{R_1 + R_2}. \quad (3)$$

The softening claw of the chisel cultivator deforms the soil towards the field surface, ie towards the open surface, and the curved claw deforms towards the side softened side, and their tensile resistance can be determined by the following expressions [3]

$$R_1 = Tt_T^{i0} b_{i0} + [k_c] \frac{\left[ b_{i0} + htg\left(\frac{\pi}{4} - \frac{\phi_2}{2}\right) \right] h}{\cos^2 \frac{1}{2}(\alpha_{i0} + \phi_1 + \phi_2)} \cos \phi_2 \sin(\alpha_{i0} + \phi_1) + b_{i0} h \rho (l_{i0} g + V^2 \sin \alpha_{i0}) tg(\alpha_{i0} + \phi_1) \left(1 + \frac{W}{100}\right), \quad (4)$$

and

$$R_2 = 2 \left\{ \frac{T t_T^y b_y}{\sin \gamma_y} + [k_c] \right\} b_y - \frac{\left[ \sqrt{[k_c]^2 + 4q_0 [k_c] b_y} \frac{tg \alpha_y \sin(\alpha_y + \varphi_1)}{\cos \varphi_y \cos(\gamma_y + \varphi_1)} - [k_c] \right] \cos(\gamma_y + \varphi) \cos \varphi_1}{2q_0 tg \alpha_y \sin(\alpha_y + \varphi_1)} \times$$

$$\times \frac{\left[ \sqrt{[k_c]^2 + 4q_0 [k_c] b_y} \frac{tg \alpha_y \sin(\alpha_y + \varphi_1)}{\cos \varphi_1 \cos(\gamma_y + \varphi_1)} - [k_c] \right]}{q_0 \sin \gamma_y tg \alpha_y \sin(\alpha_y + \varphi_1)} \times$$

$$\times [\sin(\gamma_y + \varphi_1) + \cos \gamma_y \sin \varphi_1] \cos^2 \varphi_1 + h \rho b_y \times$$

$$\times \left\{ l_y g \frac{\sin \alpha_y + (\cos \gamma_y ctg \gamma_y + \sin \gamma_y \cos \alpha_y) tg \varphi_1}{\cos \alpha_y - \sin \gamma_y \sin \alpha_y tg \varphi_1} + \right.$$

$$\left. + K_T V^2 \frac{\sin^2 \gamma_y [\sin \alpha_y + \sin \gamma_y (ctg^2 \gamma_y + \cos \alpha_y) tg \varphi_1]}{ctg \alpha_y - \sin \gamma_y tg \varphi_1} \right\} \left( 1 + \frac{W}{100} \right), \quad (5)$$

in this T – soil hardness, Па;  $t_T^{10}$  – the thickness of the softening claw blade, м; g – free fall acceleration, м/с<sup>2</sup>; ρ – soil density, кг/м<sup>3</sup>; V – the speed of movement of the chisel-cultivator during operation, м/с; W – soil moisture, %;  $t_T^y$  – the thickness of the axial claw blade, м;  $l_y$  – the width of the axial claw wing, м;  $K_T$  – in the presence of softened zones on the side of the working body ... the resistance generated by the inertial force of the soil during operation ..the coefficient taking into account the decrease in force;  $b_{10}$  – the width of the softening claw, м;  $k_c$  – specific resistance of soil to shear, Па; h – processing depth, м;  $q_0$  – coefficient of volumetric compaction of soil, H/м<sup>3</sup>;  $\alpha_{10}$ ,  $\alpha_y$  – the angle of entry of the softener and axial claws into the ground, respectively, degrees;  $\varphi_1$ ,  $\varphi_2$  – the external and internal friction angles of the soil, respectively;  $b_y$  – half of the width of the occlusal claw cover, м;  $\gamma_y$  – opening angle of axial claw wings, degrees;  $l_{10}$  – the length of the working surface of the softening claw, м.

$R_1$  and  $R_2$  We set the values of (4) and (5) to (3). In that case

$$B \leq 2 \chi \alpha_k P_H / \left\{ T t_T^{10} b_{10} + [k_c] \frac{\left[ b_{10} + h tg \left( \frac{\pi}{4} - \frac{\varphi_2}{2} \right) \right] h}{\cos^2 \frac{1}{2} (\alpha_{10} + \varphi_1 + \varphi_2)} \cos \varphi_2 \sin(\alpha_{10} + \varphi_1) + \right.$$

$$\begin{aligned}
 & + b_{10} h \rho (l_{10} g + V^2 \sin \alpha_{10}) \operatorname{tg}(\alpha_{10} + \varphi_1) \left(1 + \frac{W}{100}\right) + \\
 & + 2 \left\{ \frac{T t_T^y b_y}{\sin \gamma_y} + [k_c] b_y - \frac{\left[ \sqrt{[k_c]^2 + 4q_o [k_c] b_y} \frac{\operatorname{tg} \alpha \sin(\alpha_y + \varphi_1)}{\cos \varphi_1 \cos(\alpha_y + \varphi_1)} - [k_c] \right] \cos(\gamma_y + \varphi_1) \cos \varphi_1}{2q_o \operatorname{tg} \alpha_y \sin(\alpha_y + \varphi_1)} \right\} \times \\
 & \times \frac{\left[ \sqrt{[k_c]^2 + 4q_o [k_c] b_y} \frac{\operatorname{tg} \alpha_y \sin(\alpha_y + \varphi_1)}{\cos \varphi_1 \cos(\alpha_y + \varphi_1)} - [k_c] \right]}{q_o \sin \gamma_y \operatorname{tg} \alpha_y \sin(\alpha_y + \varphi_1)} \times \\
 & \times [\sin(\gamma_y + \varphi_1) + \cos \gamma_y \sin \varphi_1] \cos^2 \varphi_1 + h \rho b_y \times \\
 & \times \left\{ l_y g \frac{\sin \alpha_y + (\cos \gamma_y \operatorname{ctg} \gamma_y + \sin \gamma_y \cos \alpha_y) \operatorname{tg} \varphi_1}{\cos \alpha_y - \sin \gamma_y \sin \alpha_y \operatorname{tg} \varphi_1} + \right. \\
 & \left. + K_T V^2 \frac{\sin^2 \gamma_y [\sin \alpha_y + \sin \gamma_y (\operatorname{ctg}^2 \gamma_y + \cos \alpha_y) \operatorname{tg} \varphi_1]}{\operatorname{ctg} \alpha_y - \sin \gamma_y \operatorname{tg} \varphi_1} \right\} \left(1 + \frac{W}{100}\right) \}. \quad (6)
 \end{aligned}$$

$\chi = 0,9$ ;  $a = 0,2$  м,  $T = 2 \cdot 10^6$  Па,  $t_T^0 = t_T^y = 0,0005$  м,  $k_c = 2,0 \cdot 10^4$  Па,  $q_o = 10^7$  Н/м<sup>3</sup>,  $\rho = 1200$  кг/м<sup>3</sup>,  $b_{10} = 0,05$  м,  $b_y = 0,17$  м,  $h = 0,20$  м,  $l_{10} = 0,15$  м,  $f = 0,5$ ;  $l_y = 0,05$  м,  $\alpha_{10} = \alpha_y = 25^\circ$ ,  $\gamma_y = 30^\circ$ ,  $\varphi_1 = 30^\circ$ ,  $\varphi_2 = 40^\circ$ ,  $W = 16$  %,  $K_T = 0,9$ ;  $g = 9,81$  м/с<sup>2</sup> ва  $V = 2,2$  м/с Accepted and calculated according to (6), the coverage width of the chisel cultivator for aggregation with tractors ARION-630C, AXION-850, ARES-697 and NewHolland T7060 is in the range of 4.6-5.8 m, "Magnum" 8940, MX- For 255 tractors, it should be 7.2 m.

## Conclusion

The coverage width of the chisel cultivator for aggregation with high-power tractors such as Magnum 8940, MX-255, ARES-697, ARION-630C, AXION-850 and NewHolland T7060 used in the country is adjustable in the range of 4.6-7.2 m. Up to 36 working bodies should be installed.



## References

1. Тухтакузиев, А., Мансуров, М. Т., & Тошпулатов, Б. У. (2019). ИССЛЕДОВАНИЕ РАВНОМЕРНОСТИ ГЛУБИНЫ ОБРАБОТКИ ПОЧВЫ ПОЧВООБРАБАТЫВАЮЩИМИ МАШИНАМИ. In ВКЛАД УНИВЕРСИТЕТСКОЙ АГРАРНОЙ НАУКИ В ИННОВАЦИОННОЕ РАЗВИТИЕ АГРОПРОМЫШЛЕННОГО КОМПЛЕКСА (pp. 382-387).
2. Ботиров, А. Г., Негматуллаев, С. Э., & Мансуров, М. Т. (2018). ГНЕЗДУЮЩИЙ АППАРАТ СЕЯЛКИ. Экономика и социум, (5), 223-227.
3. Ботиров, А. Г., & Мансуров, М. Т. (2017). УСОВЕРШЕНСТВОВАНИЕ ПОСЕВНОЙ СЕКЦИИ. Научное знание современности, (6), 48-51.
4. Абдулхаев, Х. Г., & Мансуров, М. Т. (2017). ВЛИЯНИЕ УГЛА НАКЛОНА К ГОРИЗОНТУ ТЯГИ РОТАЦИОННОГО РЫХЛИТЕЛЯ НА ПОКАЗАТЕЛИ ЕГО РАБОТЫ. In Научно-практические пути повышения экологической устойчивости и социально-экономическое обеспечение сельскохозяйственного производства (pp. 1219-1221).
5. Мансуров, М. Т., & Расулов, А. Д. (2016). Теоретическое обоснование параметров выравнителя-уплотнителя комбинированной машины по системе push-pull для предпосевной обработки почвы. Молодой ученый, (8), 256-259.
6. Tukhtakuziyev, A., & Mansurov, M. T. (2015). Research of stability of tractor with front and rear-mounted tools against sidewise skidding. Tractors and Agricultural Machinery, (9), 34-35.
7. Tuhtakuziev, A., & Mansurov, M. T. (2015). Issledovanie ustojchivosti traktora s orudijami perednej i zadnej naveski protiv bokovogo zanosa. Traktory i sel'hozmashiny, (9), 34-35.
8. Tukhtakuziev, A., & Mansurov, M. T. (2015). Research of resistance on the tractor equipped with implements at front and backside lift hitch contrarily the sidewise skidding. Europaische Fachhochschule, (6), 76-77.
9. Tuhtakuziev, A., & Mansurov, M. T. (2015). Issledovanie ustojchivosti traktora s orudijami perednej i zadnej naveski protiv bokovogo zanosa. Traktory i sel'hozmashiny, (9), 34-35.
10. Мансуров, М. Т., & Тухтакузиев, А. (2015). Исследование устойчивости трактора с орудиями передней и задней навески против бокового заноса. Тракторы и сельхозмашины.-2015.-№ 10.-С. 34-35.



11. Тухтакузиев, А., & Мансуров, М. Т. (2015). Исследование устойчивости трактора с орудиями передней и задней навески против бокового заноса. Тракторы и сельхозмашины, (9), 34-35.
12. Тухтакузиев, А., & Мансуров, М. Т. (2015). Исследование устойчивости прямолинейного движения трактора с орудиями передней и задней навески. In Интеллектуальные машинные технологии и техника для реализации Государственной программы развития сельского хозяйства (pp. 125-128).
13. Тухтакузиев, А., & Мансуров, М. Т. (2015). Исследование устойчивости прямолинейного движения трактора с орудиями передней и задней навески. In Интеллектуальные машинные технологии и техника для реализации Государственной программы развития сельского хозяйства (pp. 125-128).
14. Тухтакузиев, А., Мансуров, М., Расулжонов, А., & Каримова, Д. Научные основы обеспечения равномерности глубины работы почвообрабатывающих машин. Ташкент: Издательство TURON-IQBOL.–2020.
15. Абдулхаев, Х. Г., & Мансуров, М. Т. (2017). Влияние угла наклона к горизонту тяги ротационного рыхлителя на показатели его работы. In Научно-практические пути повышения экологической устойчивости и социально-экономическое обеспечение сельскохозяйственного производства (pp. 1219-1221).
16. Мансуров, М. Т., & Тухтакузиев, А. (2015). Исследование устойчивости трактора с орудиями передней и задней навески против бокового заноса. Тракторы и сельхозмашины.-2015.-№ 10.-С. 34-35.
17. Tukhtakuziev, A., & Mansurov, M. T. (2015). Research of resistance on the tractor equipped with implements at front and backside lift hitch contrarily the sidewise skidding. Europaische Fachhochschule, (6), 76-77.
18. Тухтакузиев, А., Мансуров, М., Расулжонов, А., & Каримова, Д. Научные основы обеспечения равномерности глубины работы почвообрабатывающих машин. Ташкент: Издательство TURON-IQBOL.–2020
19. Мансуров М.Т. Научно-технические решения агрегатирования почвообрабатывающих машин, состоящих из рабочих частей, навешиваемых спереди и сзади на колесные тракторы. Автореферат дисс. ... доктора техн. наук (DSc). – Ташкент, 2018. – 54 с.
20. <https://www.indianjournals.com/ijor.aspx?target=ijor:aca&volume=11&issue=6&article=102>